

So, \vec{n} is:

$$\vec{n} = \frac{\vec{r}_r \times \vec{r}_\theta}{\|\vec{r}_r \times \vec{r}_\theta\|} = \frac{\langle -2r^2 \cos \theta, -2r^2 \sin \theta, r \rangle}{r \sqrt{4r^2 + 1}}$$

Lecture 21

Flux:

21-1

The concept of flux is measuring the rate at which something flows through a surface (e.g. air through a butterfly net).

$$d\vec{S} = \vec{n} dS = \frac{\vec{r}_u \times \vec{r}_v}{\|\vec{r}_u \times \vec{r}_v\|} (\cancel{\|\vec{r}_u \times \vec{r}_v\|} dA) = (\vec{r}_u \times \vec{r}_v) dA$$

Def: If \vec{F} is a continuous vector field defined on a surface S which has orientation \vec{n} , then the flux of \vec{F} across S is

$$\iint_S \vec{F} \cdot d\vec{S} = \iint_S (\vec{F} \cdot \vec{n}) dS$$

$$\left[\begin{array}{l} S \text{ parametrized by } \vec{r}(u,v) \\ \vec{n} = \frac{\vec{r}_u \times \vec{r}_v}{\|\vec{r}_u \times \vec{r}_v\|} \end{array} \right] = \iint_D \vec{F}(\vec{r}(u,v)) \cdot (\vec{r}_u \times \vec{r}_v) dA$$

Ex: Find the flux of $\vec{F} = \langle x, y, z \rangle$ across the helicoid parametrized by $\vec{r}(u, v) = \langle u \cos v, u \sin v, v \rangle$, $0 \leq u \leq 1$, $0 \leq v \leq \frac{\pi}{2}$ with upward orientation.

Sol: Start by finding the correct orientation.

$$\vec{r}_u = \langle \cos v, \sin v, 0 \rangle, \quad \vec{r}_v = \langle -u \sin v, u \cos v, 1 \rangle$$

$$\vec{r}_u \times \vec{r}_v = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \cos v & \sin v & 0 \\ -u \sin v & u \cos v & 1 \end{vmatrix} = \langle \sin v, -\cos v, u \rangle$$

Since the \hat{k} -component is positive, we have the right order. Since $\|\vec{r}_u \times \vec{r}_v\|$ cancels out in the flux integral there's no need to compute it.

$$\vec{F}(\vec{r}(u, v)) = \langle u \cos v, u \sin v, v \rangle$$

$$\vec{F}(\vec{r}(u, v)) \cdot (\vec{r}_u \times \vec{r}_v) = u \cos v \sin v - u \sin v \cos v + uv = uv$$

So, the flux is:

$$\begin{aligned} \iint_S \vec{F} \cdot d\vec{S} &= \int_0^1 \int_0^{\pi/2} uv \, dv \, du = \int_0^1 \frac{1}{2} uv^2 \Big|_0^{\pi/2} du = \int_0^1 \frac{\pi^2}{8} u \, du \\ &= \frac{\pi^2}{16} \end{aligned}$$

□

Ex: Compute $\iint_S \vec{F} \cdot d\vec{S}$ where $\vec{F} = \text{curl } \vec{G}$,

$\vec{G} = \langle -2yz, y, 3x \rangle$, and S is the piece of the paraboloid $z = 5x^2 - y^2$ above the plane $z = 1$, with upward orientation.

Sol: Begin by parametrizing S . Using cylindrical, the paraboloid is $z = 5 - r^2$, so:

$$x = r \cos \theta$$

$$y = r \sin \theta$$

$$z = z = 5 - r^2, \quad 0 \leq \theta \leq 2\pi, \quad 0 \leq r \leq ?$$

To get the upper bound on r , we need to know the intersection of the paraboloid with $z = 1$:

$$1 = z = 5 - x^2 - y^2 \Leftrightarrow x^2 + y^2 = 4 \Leftrightarrow r = 2$$

So, a parametrization is

$$\vec{r}(r, \theta) = \langle r \cos \theta, r \sin \theta, 5 - r^2 \rangle, \quad 0 \leq r \leq 2, \quad 0 \leq \theta \leq 2\pi$$

$$\text{Now, } \vec{r}_r = \langle \cos \theta, \sin \theta, -2r \rangle, \quad \vec{r}_\theta = \langle -r \sin \theta, r \cos \theta, 0 \rangle$$

$$\vec{r}_r \times \vec{r}_\theta = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \cos \theta & \sin \theta & -2r \\ -r \sin \theta & r \cos \theta & 0 \end{vmatrix} = \langle 2r^2 \cos \theta, 2r^2 \sin \theta, r \rangle$$

Since the \hat{k} -component is positive, this was the correct order.

Now,

$$\vec{F} = \text{curl } \vec{G} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ -2yz & y & 3x \end{vmatrix} = \langle 0, -2y-3, 2z \rangle$$

So,

$$\vec{F}(\vec{r}(r, \theta)) = \langle 0, -2r\sin\theta - 3, 10 - 2r^2 \rangle$$

and

$$\vec{F}(\vec{r}(r, \theta)) \cdot (\vec{r}_r \times \vec{r}_\theta) = -4r^3 \sin^2\theta - 6r^2 \sin\theta + 10r - 2r^3$$

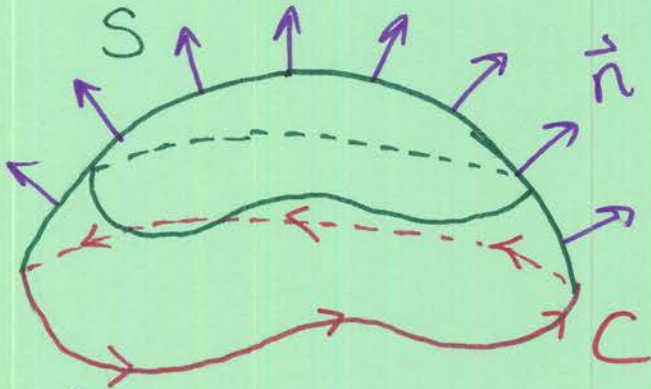
Finally,

$$\begin{aligned} \iint_S \vec{F} \cdot d\vec{S} &= \int_0^{2\pi} \int_0^2 (-4r^3 \sin^2\theta - 6r^2 \sin\theta + 10r - 2r^3) dr d\theta \\ &= \int_0^{2\pi} \left(-r^4 \sin^2\theta - 2r^3 \sin\theta + 5r^2 - \frac{1}{2}r^4 \right) \Big|_0^2 d\theta \\ &= \int_0^{2\pi} (-16\sin^2\theta - 16\sin\theta + 12) d\theta \quad \left(\sin^2\theta = \frac{1 - \cos 2\theta}{2} \right) \\ &= \int_0^{2\pi} (8\cos 2\theta - 16\sin\theta + 4) d\theta \\ &= (4\sin 2\theta + 16\cos\theta + 4\theta) \Big|_0^{2\pi} = 8\pi \quad \diamond \end{aligned}$$

16.8 - Stokes' Theorem

Let S be a surface with boundary C and orientation \vec{n} :

ex:



We say that C has orientation consistent with S if while traversing C with your head in the direction of \vec{n} , the surface is on your left. In this sense, we say S induces an orientation on C , and C with this orientation is denoted ∂S .

Stokes' Theorem: Let S be an oriented, piecewise-smooth surface which is bounded by a simple, closed, piecewise-smooth curve C , and give C the orientation induced by S . Let \vec{F} be a vector field on \mathbb{R}^3 which is C^1 in an open region containing S . Then

$$\int_C \vec{F} \cdot d\vec{r} = \iint_S (\text{curl } \vec{F}) \cdot d\vec{S}$$

Let's revisit the example from earlier:

Alt. Sol.:

We can apply Stokes' theorem to this case. C is the circle $x^2 + y^2 = 4, z = 1$. The orientation we want on C is the counterclockwise one, when viewed from above. So, a parametrization of C is:

$$\vec{r}(t) = \langle 2\cos t, 2\sin t, 1 \rangle, \quad 0 \leq t \leq 2\pi.$$

By Stokes':
$$\iint_S \text{curl } \vec{G} \cdot d\vec{S} = \int_C \vec{G} \cdot d\vec{r},$$

so:
$$\vec{G}(\vec{r}(t)) = \langle -4\sin t, 2\sin t, 6\cos t \rangle$$

$$\vec{r}'(t) = \langle -2\sin t, 2\cos t, 0 \rangle$$

$$\vec{G}(\vec{r}(t)) \cdot \vec{r}'(t) = 8\sin^2 t + 4\sin t \cos t$$

$$\int_C \vec{G} \cdot d\vec{r} = \int_0^{2\pi} (8\sin^2 t + 4\sin t \cos t) dt$$

$$= \int_0^{2\pi} (4 - 4\cos 2t + 4\sin t \cos t) dt$$

$$= (4t - \sin t + 2\sin^2 t) \Big|_0^{2\pi} = 8\pi$$



Quicker!

Ex: Compute $\int_C \vec{F} \cdot d\vec{r}$ where $\vec{F} = \langle xy, 2z, 3y \rangle$ and C is the curve of intersection between $x+z=5$ and $x^2+y^2=9$, oriented counterclockwise when viewed from above.

Sol: Parametrizing C wouldn't be too bad

$$\vec{r}(t) = \langle 3\cos t, 3\sin t, 5-3\cos t \rangle, 0 \leq t \leq 2\pi$$

but: $\vec{r}'(t) = \langle -3\sin t, 3\cos t, 3\sin t \rangle$

& $\vec{F}(\vec{r}(t)) = \langle 9\cos t \sin t, 10-6\cos t, 9\sin t \rangle$

so:

$$\vec{F}(\vec{r}(t)) \cdot \vec{r}'(t) = -27\cos t \sin^2 t + 30\cos t - 18\cos^2 t + 27\sin^2 t \dots$$

awful...

But, we can still use Stokes' theorem! We need a surface with boundary on C . We may as well use the piece of the plane $x+z=5$ inside the cylinder $x^2+y^2=9$. So:

$$\vec{r}(x,y) = \langle x, y, 5-x \rangle, D = \{x^2+y^2 \leq 9\}$$

In order for S to induce the correct orientation on C , it needs the upward orientation. So:

$\vec{r}_x = \langle 1, 0, -1 \rangle, \vec{r}_y = \langle 0, 1, 0 \rangle$, which has positive \hat{k} -component, so $\vec{r}_x \times \vec{r}_y$ is the correct order

$$\vec{r}_x \times \vec{r}_y = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 1 & 0 & -1 \\ 0 & 1 & 0 \end{vmatrix} = \langle 1, 0, 1 \rangle,$$

$$\text{curl } \vec{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ xy & 2z & 3y \end{vmatrix} = \langle 1, 0, -x \rangle, (\text{curl } \vec{F})(\vec{r}(x,y)) = \langle 1, 0, -x \rangle.$$

Thus,

$$\begin{aligned}
 \int_C \vec{F} \cdot d\vec{r} &= \iint_S \text{curl } \vec{F} \cdot d\vec{S} = \iint_D \langle 1, 0, -x \rangle \cdot \langle 1, 0, 1 \rangle dA \\
 &= \iint_D (1-x) dA \stackrel{\substack{\text{switch to} \\ \text{polar}}}{=} \int_0^{2\pi} \int_0^3 (1-r\cos\theta) r dr d\theta \\
 &= \int_0^{2\pi} \int_0^3 (r - r^2 \cos\theta) dr d\theta = \int_0^{2\pi} \left(\frac{r^2}{2} - \frac{r^3}{3} \cos\theta \right) \Big|_0^3 d\theta \\
 &= \int_0^{2\pi} \left(\frac{9}{2} - 9\cos\theta \right) d\theta = 9\pi. \quad \diamond
 \end{aligned}$$

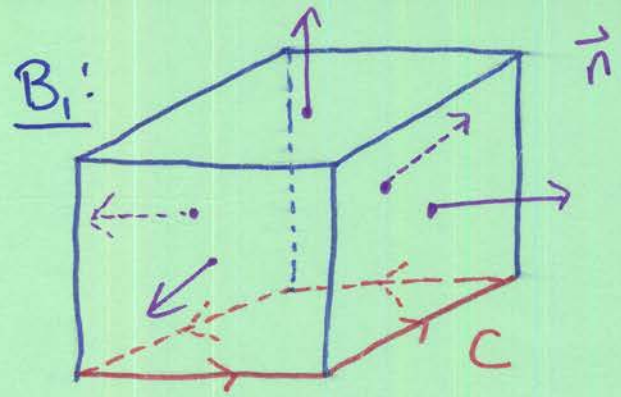
Let's close with one more example: a trick.

Suppose S_1 & S_2 have the same boundary C , and they both induce the same orientation on C . If everything in question satisfies Stokes' theorem, then

$$\iint_{S_1} (\text{curl } \vec{F}) \cdot d\vec{S} = \int_C \vec{F} \cdot d\vec{r} = \iint_{S_2} (\text{curl } \vec{F}) \cdot d\vec{S}.$$

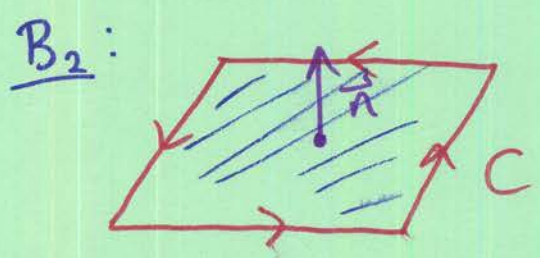
I like to call this process "surface swapping".

Suppose we were asked to compute $\iint_{B_1} (\text{curl } \vec{F}) \cdot d\vec{S}$, where B_1 is the surface of the box $[0,1] \times [0,1] \times [0,1]$, with no bottom, where B_1 has the "outward" orientation.



This would require computing 5 surface integrals... quite frustrating, and switching to an integral over the boundary C still requires 4 line integrals...

However, using surface swapping, we can replace B₁ by the bottom of the box, B₂, with upward orientation:



$$B_2 = [0, 1] \times [0, 1] \times \{0\}$$

Much easier!